

Experiences from Vertical Full Scale Castings with SCC

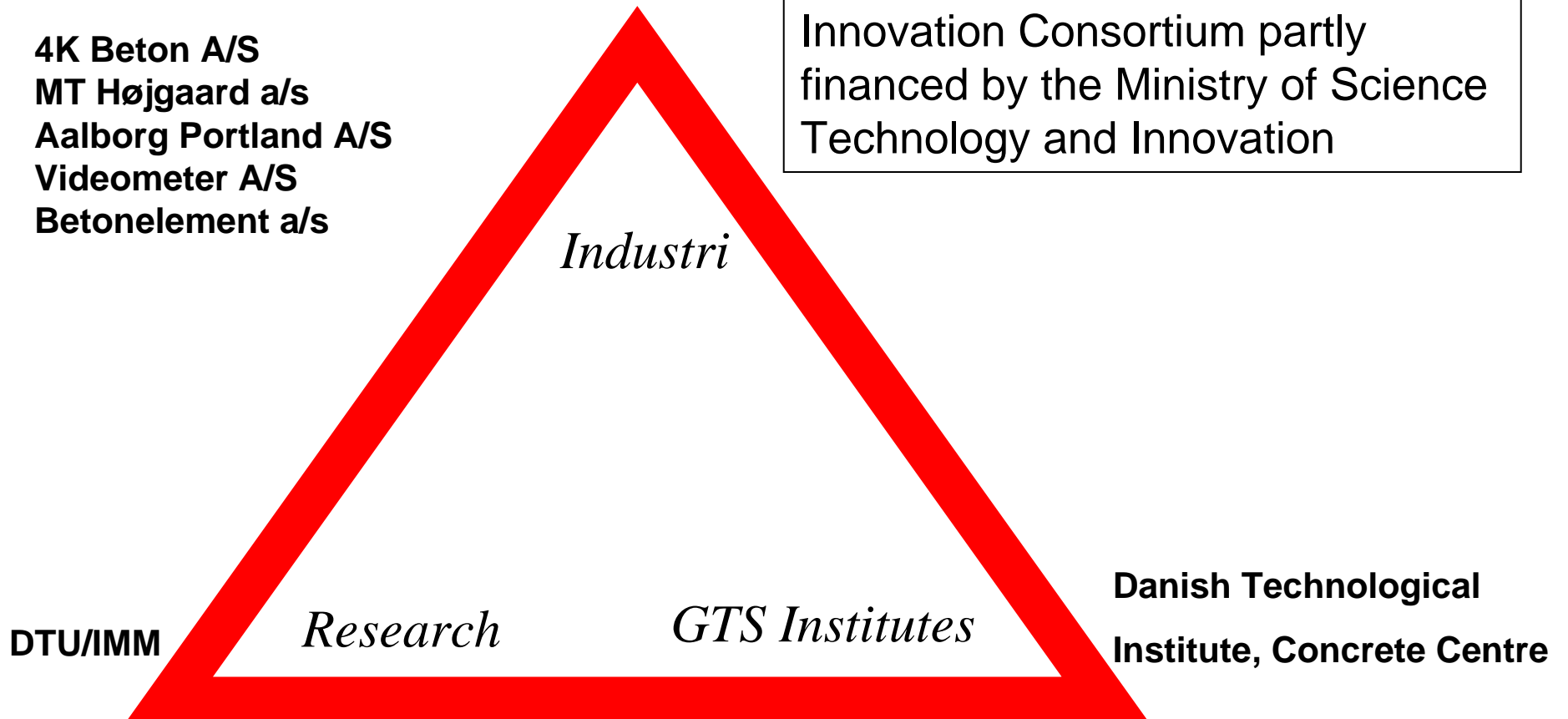
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SCC Consortium

4K Beton A/S
MT Højgaard a/s
Aalborg Portland A/S
Videometer A/S
Betonelement a/s

Innovation Consortium partly
financed by the Ministry of Science
Technology and Innovation



Overall objective:

To improve the productivity and the working environment of the concrete industry

Outline

Introduction

Test setup

Results

- Form filling
 - Segregation/Blocking
 - Form pressure
 - Surface finish
 - Frost resistance
 - Air void structure
- Fresh state
- Hardened state

Introduction

The use of SCC in vertical castings is still much lower than the use of SCC use in horizontal castings such as floors.

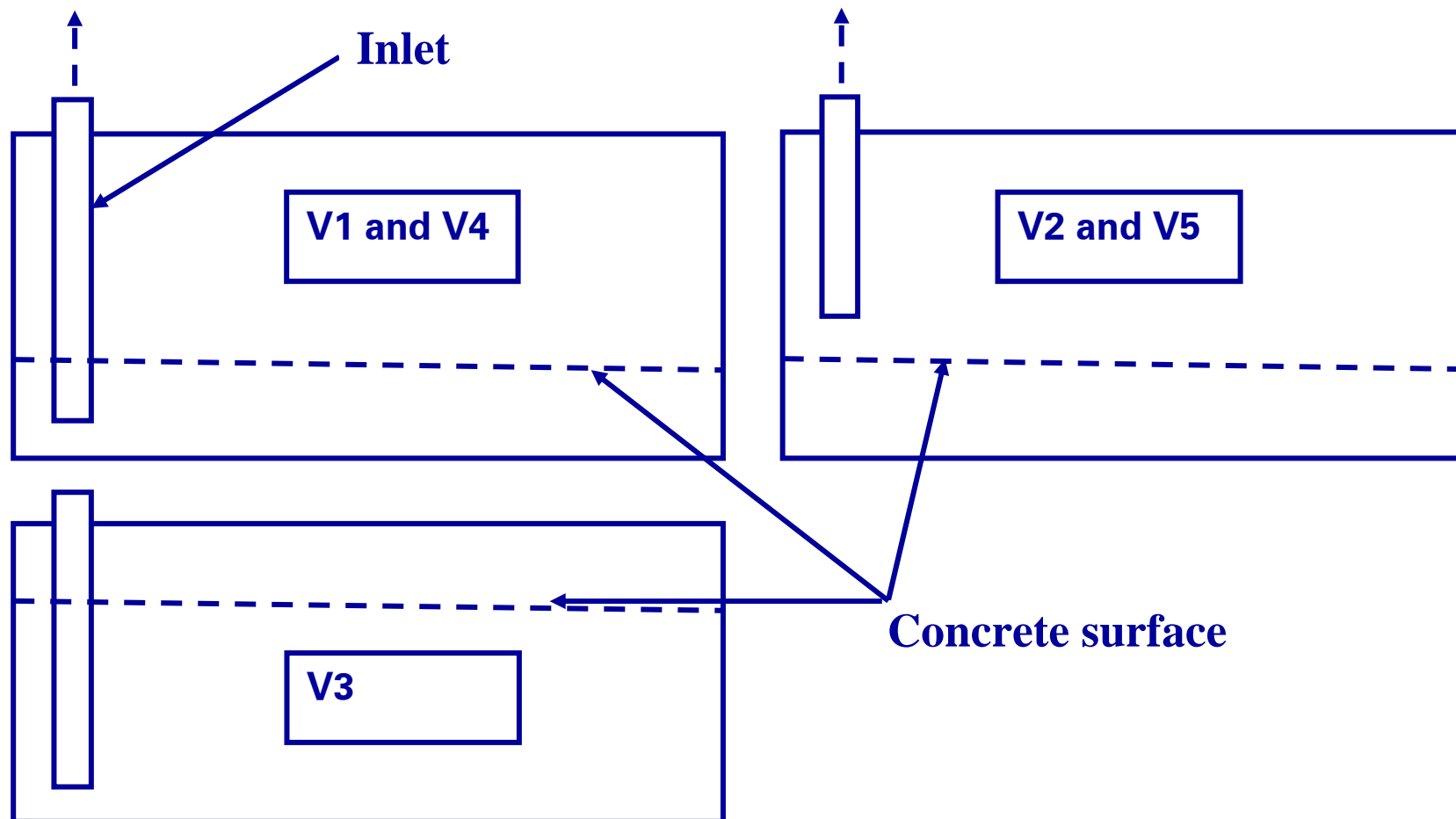
The aim of the full scale wall castings is to obtain experience on i.e.

- the relation between the fresh concrete workability, casting technique and the form filling behavior
- form pressure
- surface finish
- air void structure and frost resistance

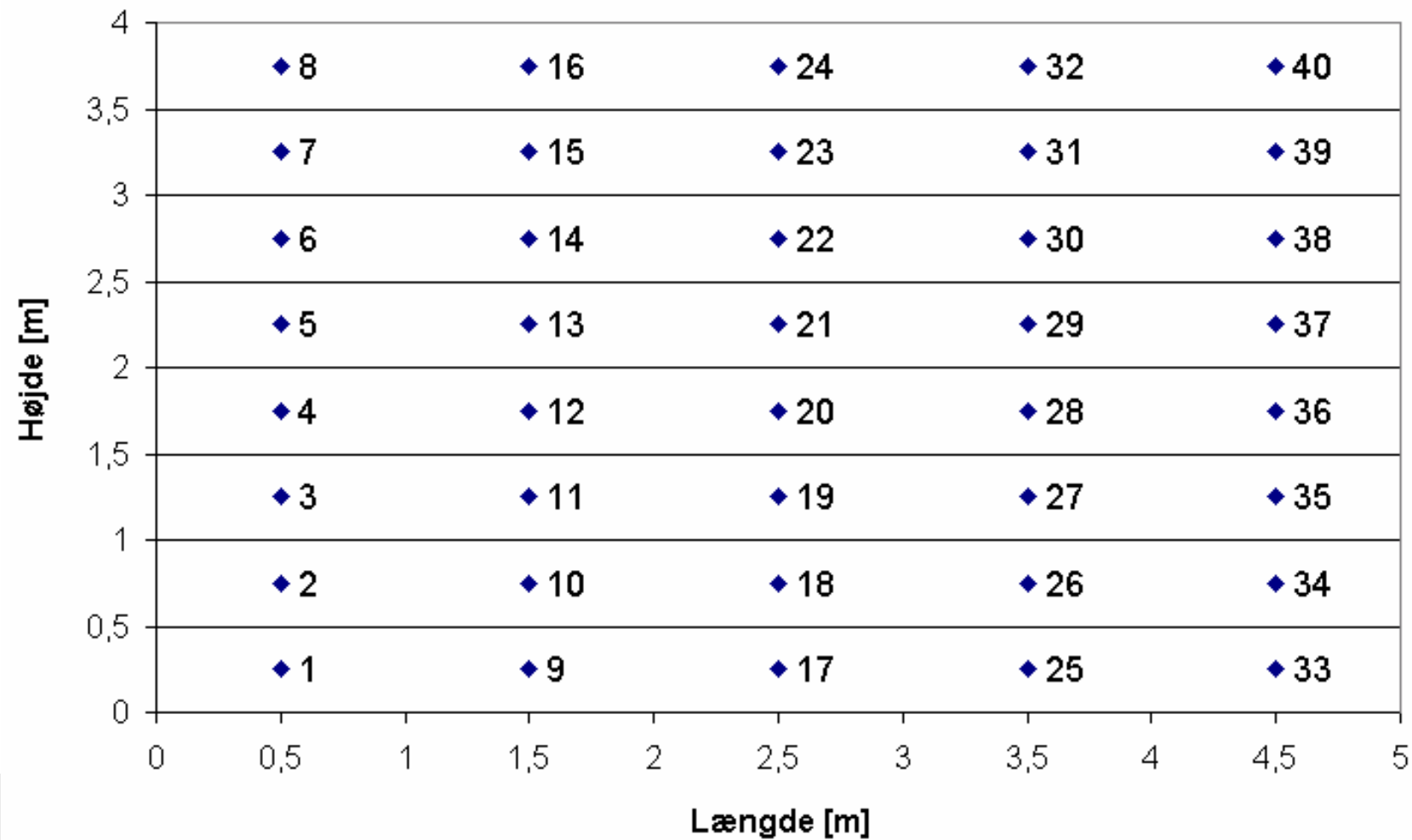
Test Setup

Wall ID	V1	V2	V3	V4	V5
Dimensions	H * W * L = 4m * 0.5m * 5m				
Concrete Type	A35	A35	A35	M30	M30

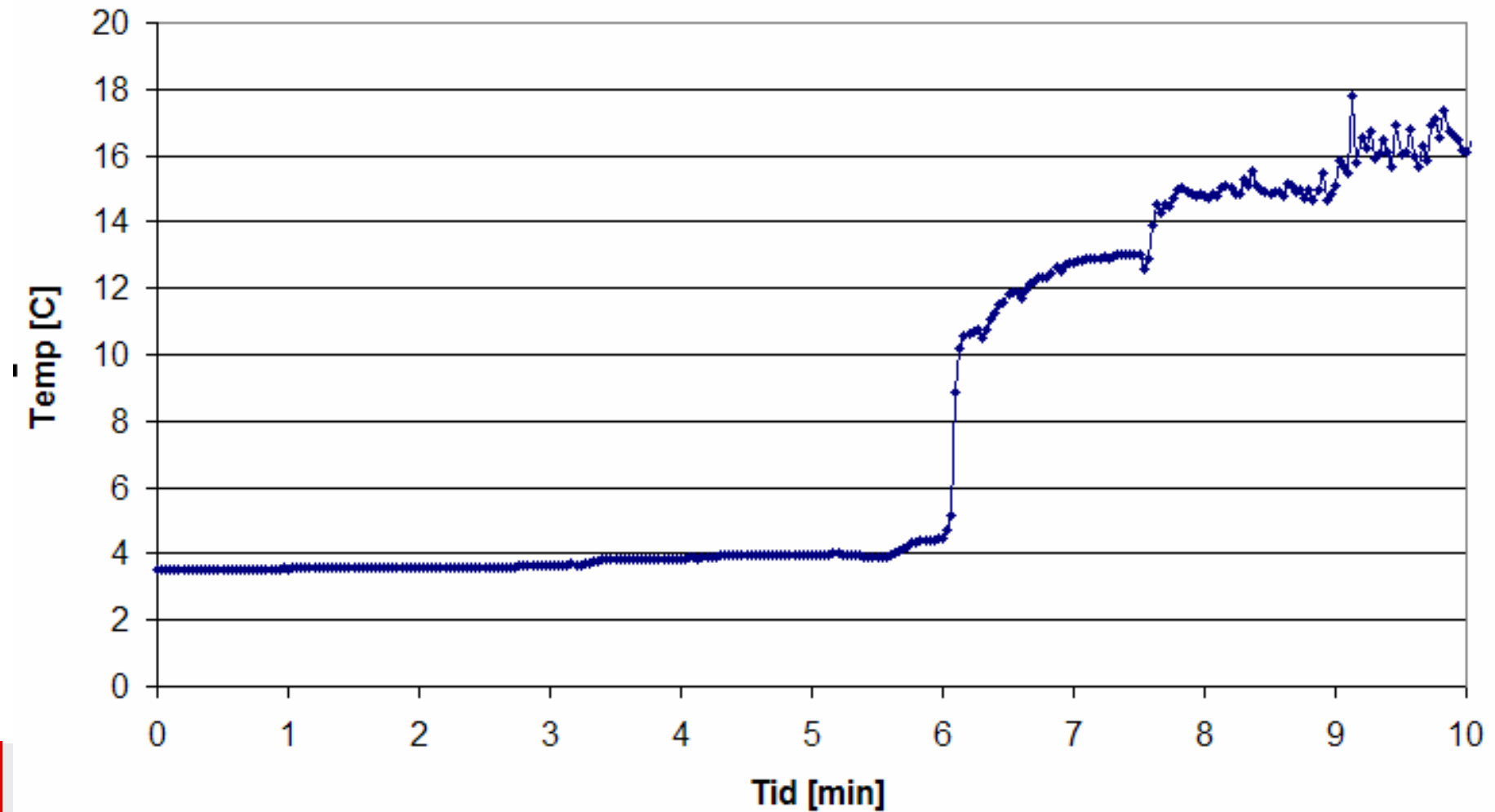
Test Setup



Test Setup



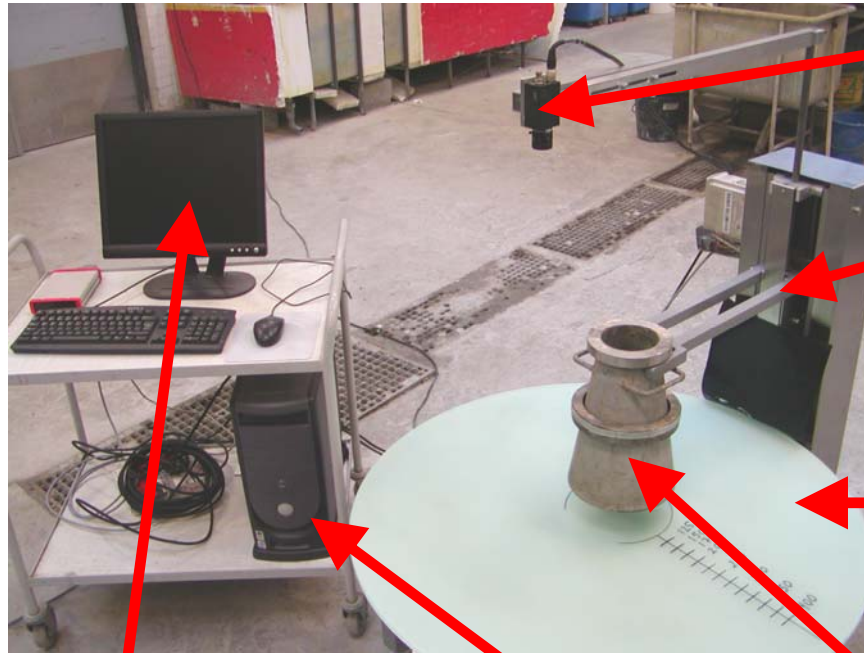
Test Setup



Test Setup

Slump Flow, Annex U i DS 2426	Compressive strength
Slump Flow, 4C Auto-slump	Heat development
J-ring	Finish
Air content	Macro analysis
Air void distribution: Air-Void-meter	Air void structure: EN 480-11
Form pressure	Frost Resistance: SS 13 72 44
Temperature	

4C Automatic Slump Flow



B/W Video camera

Lifting device – Ball screw ensures accurate lifting speed of 7 cm/s

Base plate in hardened sand blasted glass on adjustable rubber feet

Everything mounted on "rollers"

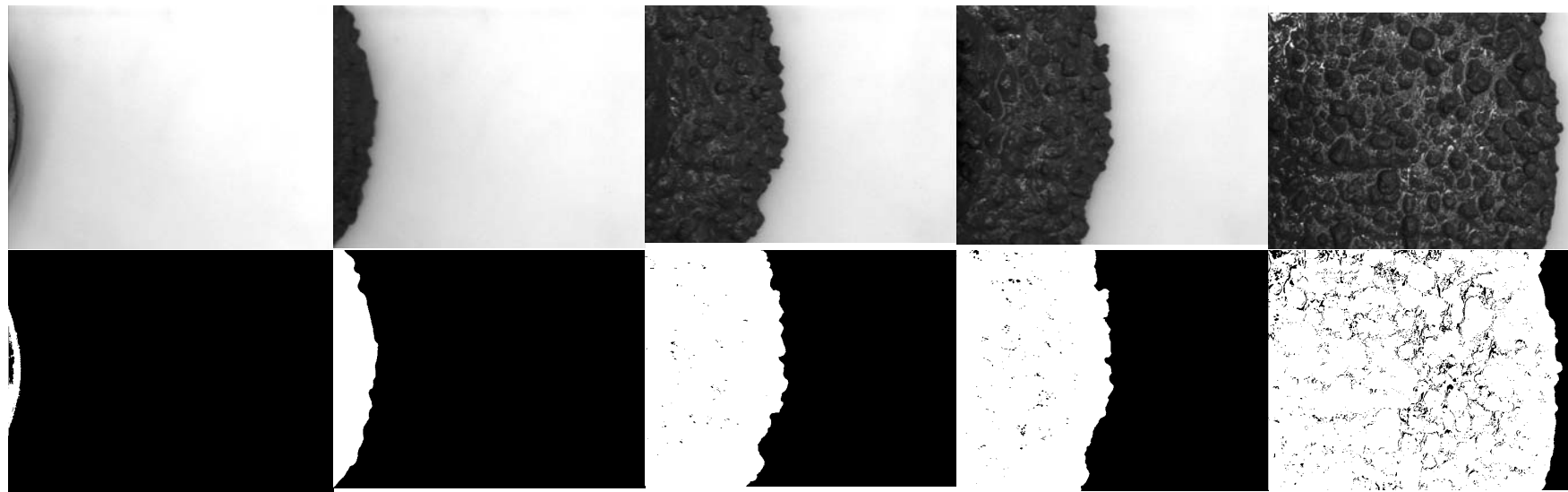
Monitor – one click and the analysis will proceed automatically

PC

Upright Abrams slump cone with weight ring

4C Automatic Slump Flow

Concept:



Field of view 232 x 172mm – 640 x 480 pixels

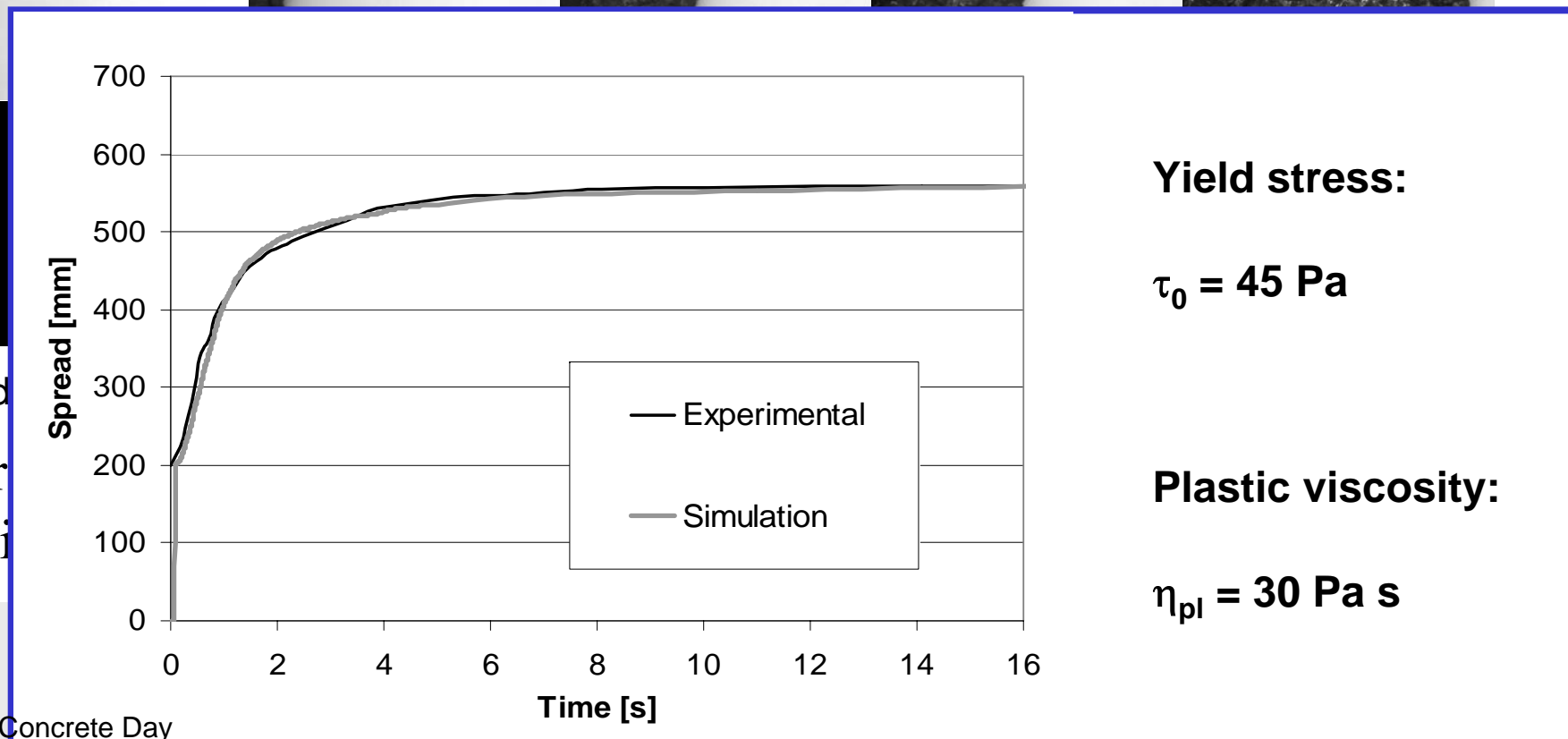
Spread as a function of time is determined –
30 images per second

Binary image –
only black and
white pixels

4C Automatic Slump Flow

Concept:

Raw image



Yield stress:

$$\tau_0 = 45 \text{ Pa}$$

Plastic viscosity:

$$\eta_{pl} = 30 \text{ Pa s}$$

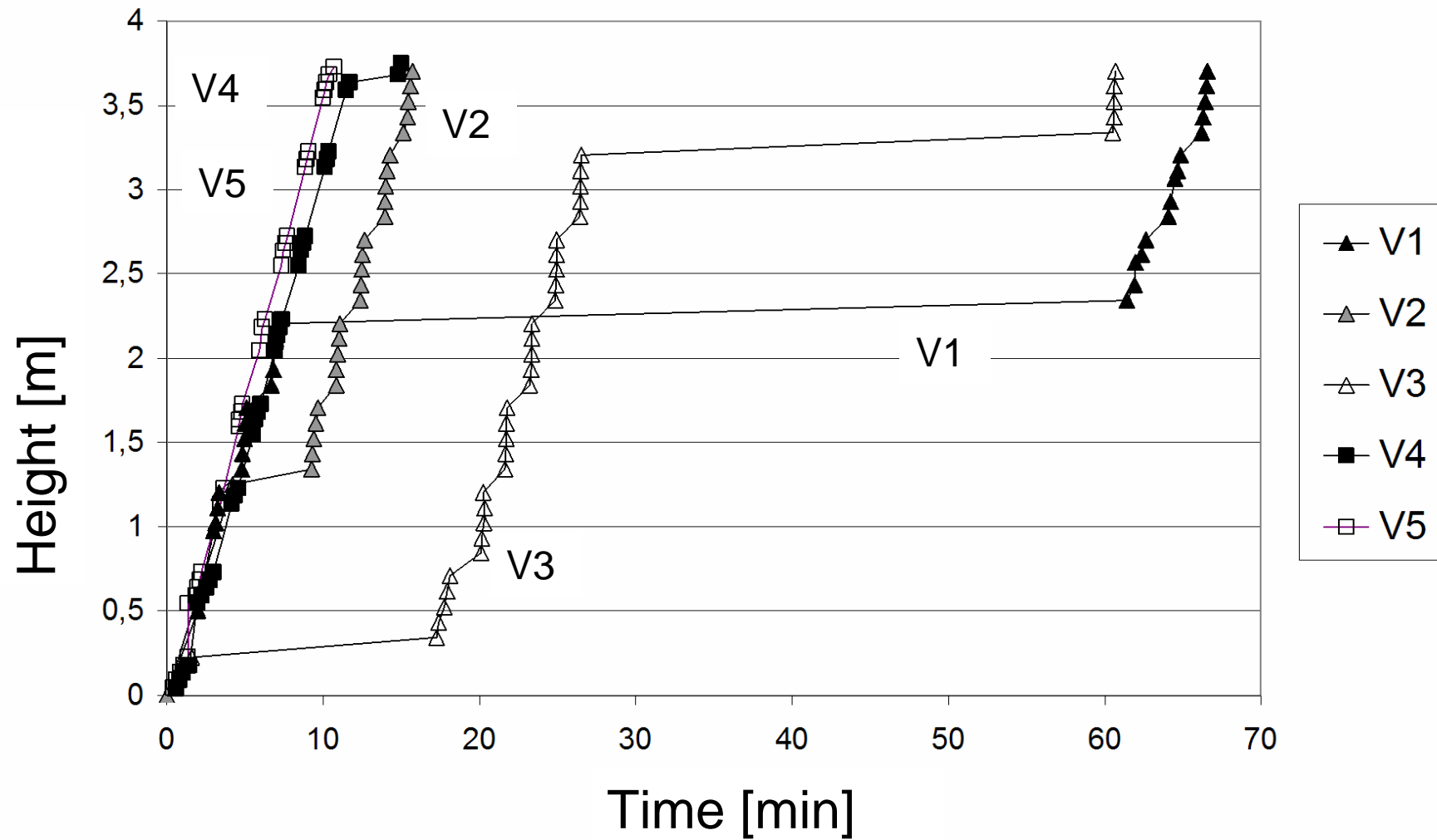
Field
Spr
30 i



Results

	V1	V2	V3	V4	V5
Air [%]	5	6.6	5.1	8.5	7.1
SF [mm]	640	660	670	550	570
τ_0 [Pa]	20			60	45
η_{pl} [Pa·s]	60			34	34

Results

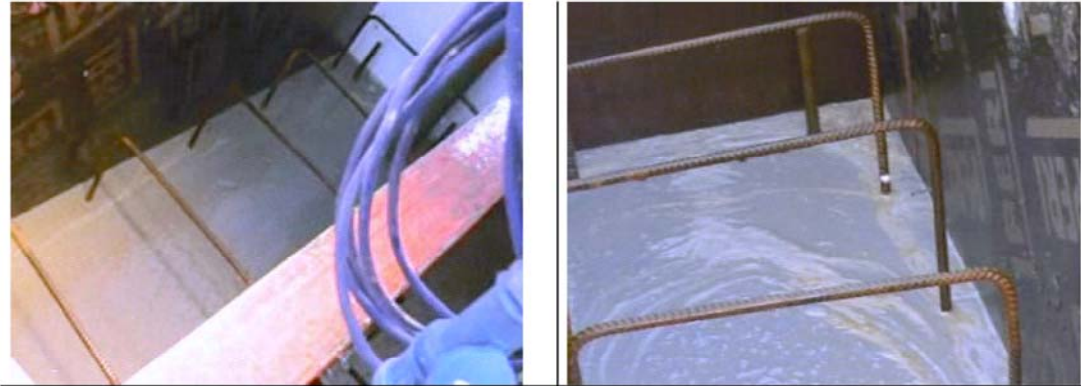


Results

Complete form filling was obtained. Depending on the rheological properties it was necessary to move the inlet to level the concrete surface.

Form geometry and reinforcement configuration do not prevent high casting rates of up to 25 m/hour. However, may have to lower due to e.g. finish and form pressure.

Results

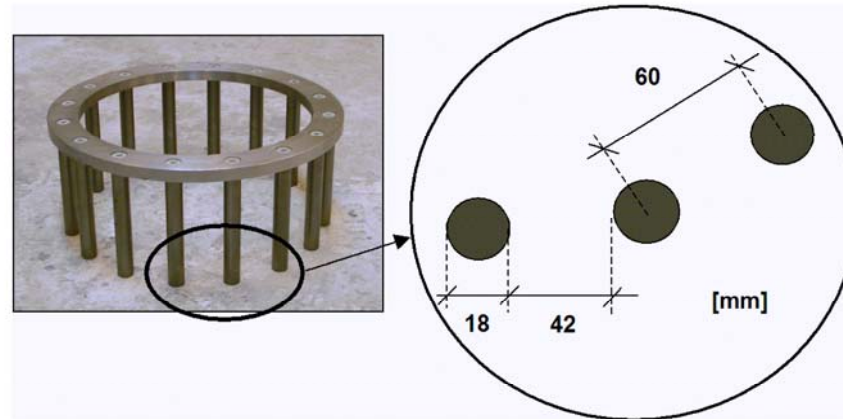


V1 (~ 2 cm)



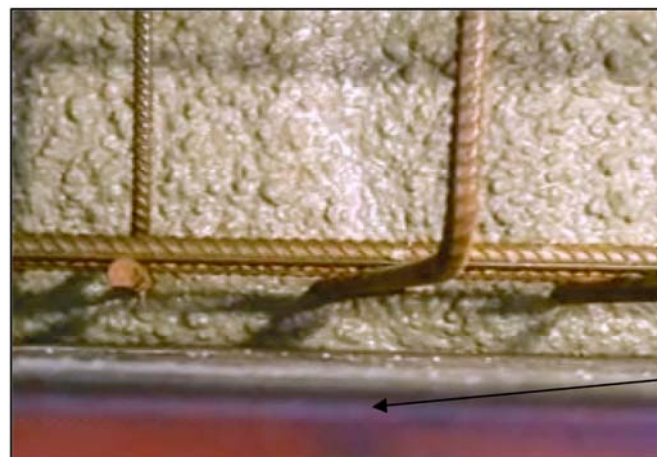
V4 (~ 10 cm)

Results



2.6

Blocking was not observed during form filling.



3.2

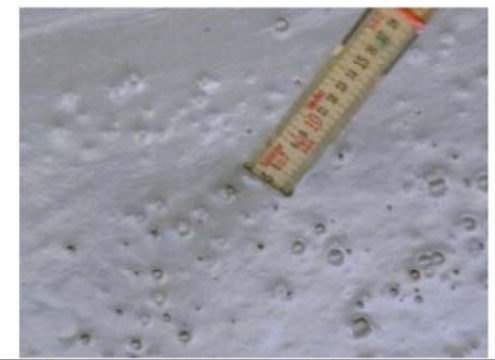
Res



V4 (0 cm)



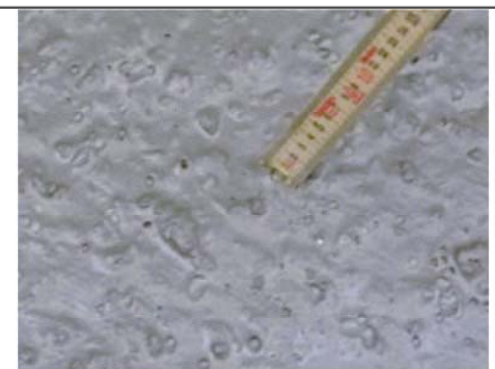
V1 (~ 5 cm)



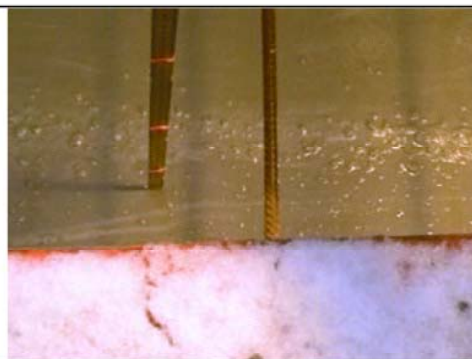
V5 (0 cm)



V2 (~ 0 cm)



Dynamic segregation very dependent on the casting technique and the rheological properties.

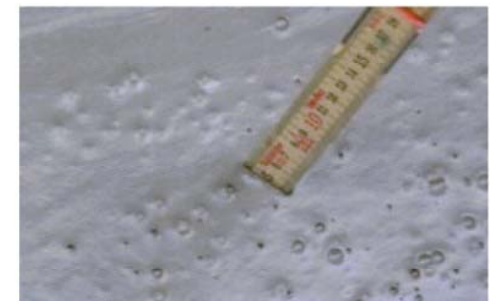


V3 (~ 10 cm)

Res

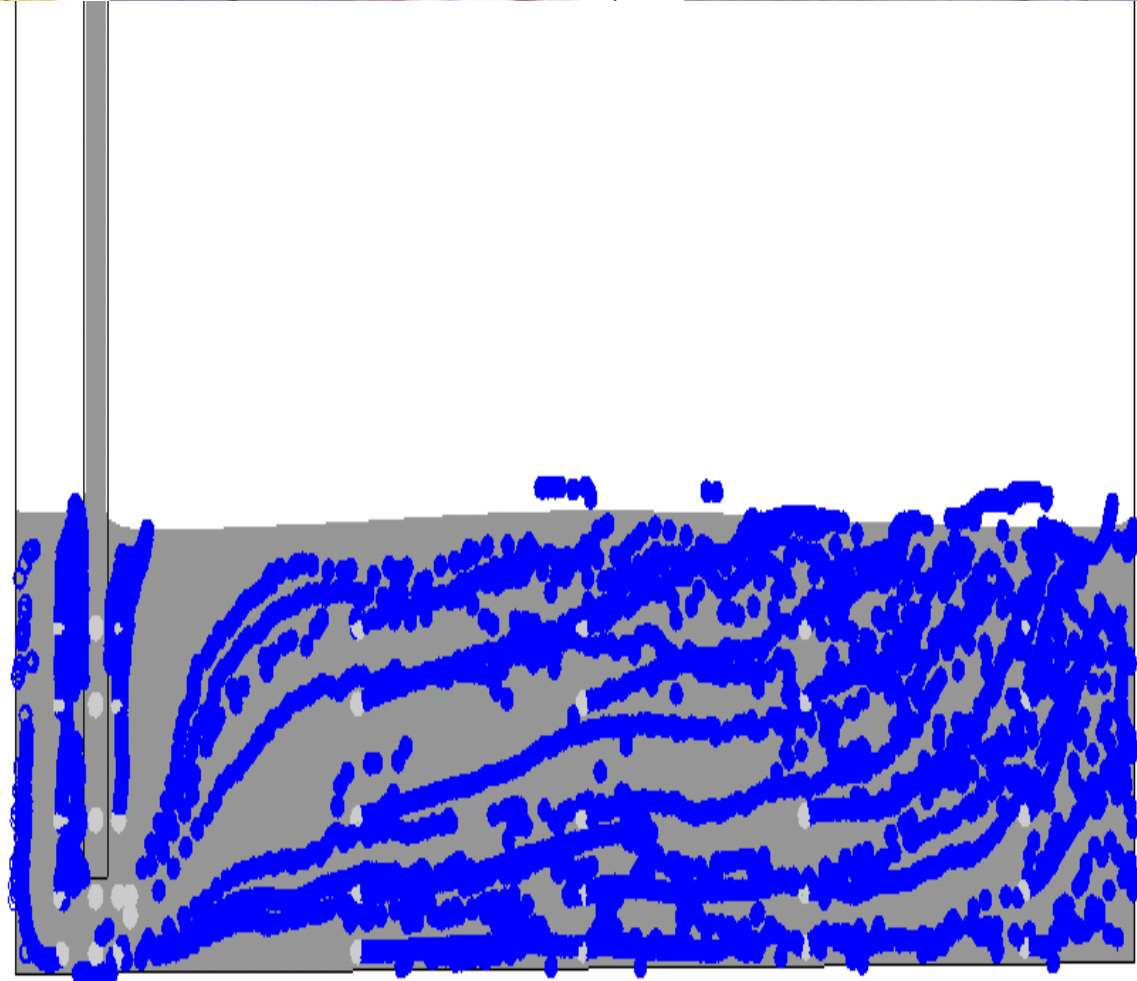


V4 (0 cm)



V5 (0 cm)

Dynamic segregation very dependent on the casting technique and the rheological properties.



V3 (~ 10 cm)

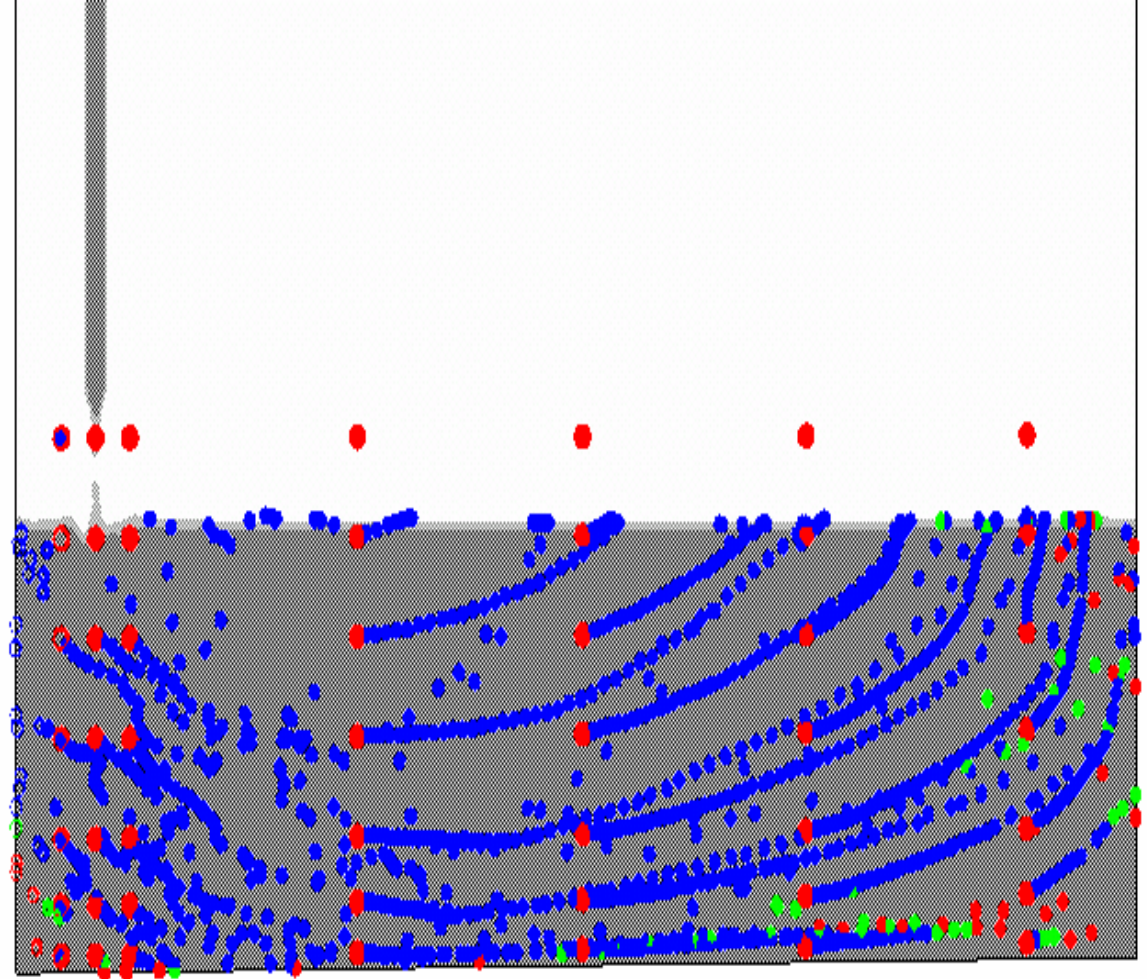
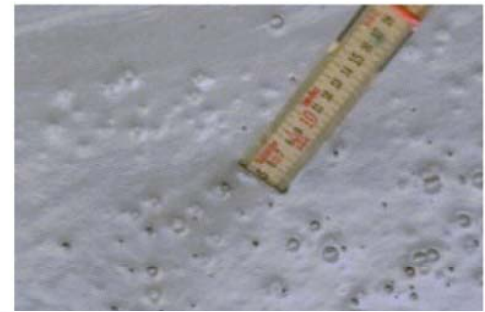
Res



V4 (0 cm)



V5 (0 cm)

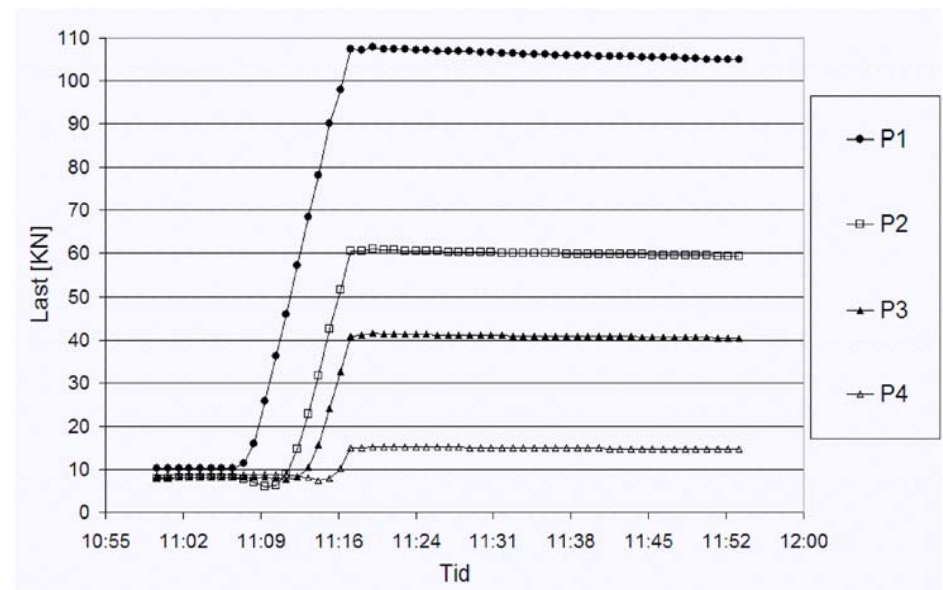
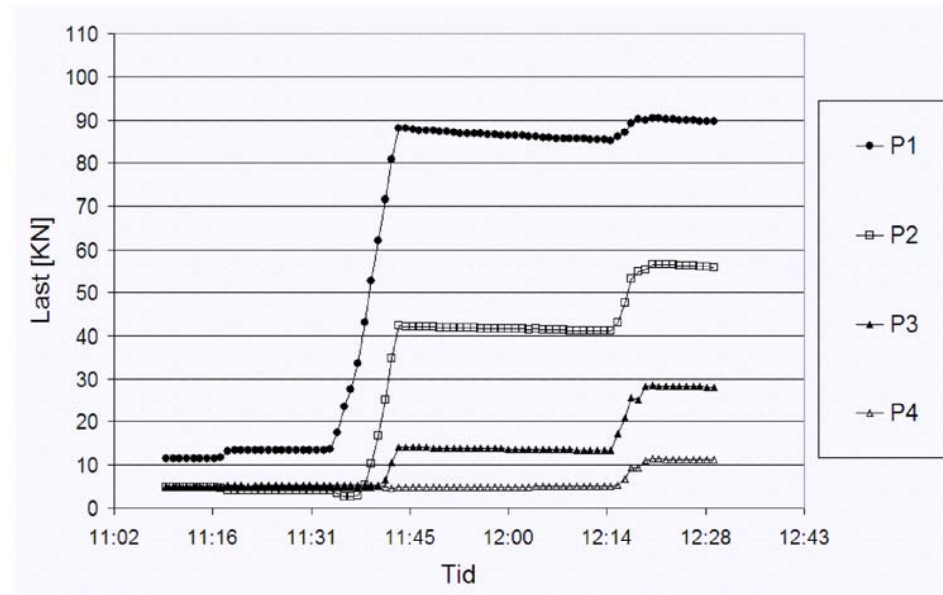
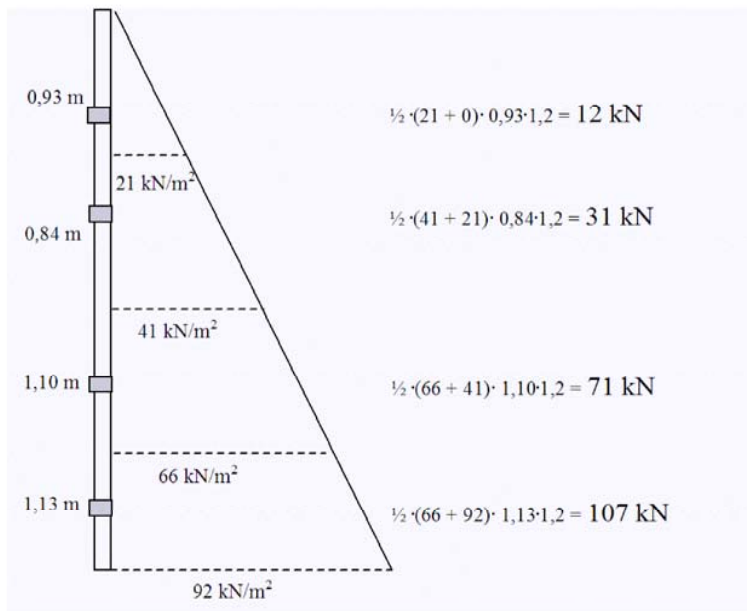


V3 (~ 10 cm)

Dynamic segregation very dependent on the casting technique and the rheological properties.

Results

Hydrostatic pressure is obtained (> 18 m/hour)



Results

2 types of form oil:

- Bricon Unislip 9-12, mineral oil
- Emulfix LL, vegetable formolie

Visual inspection showed no difference in surface finish.

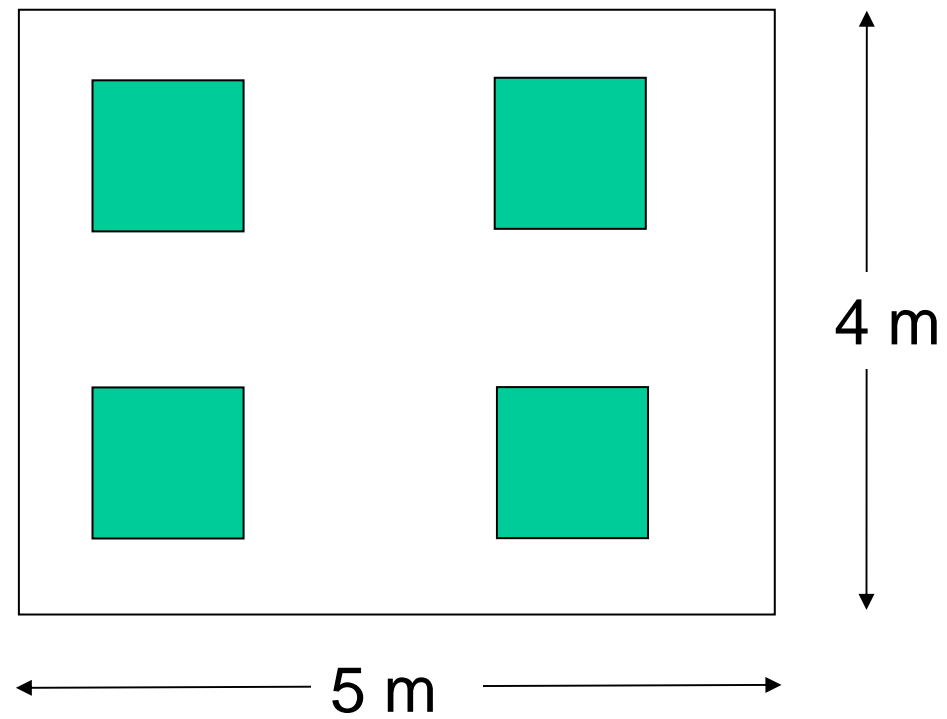
Results

Finish is evaluated by counting pores according to:

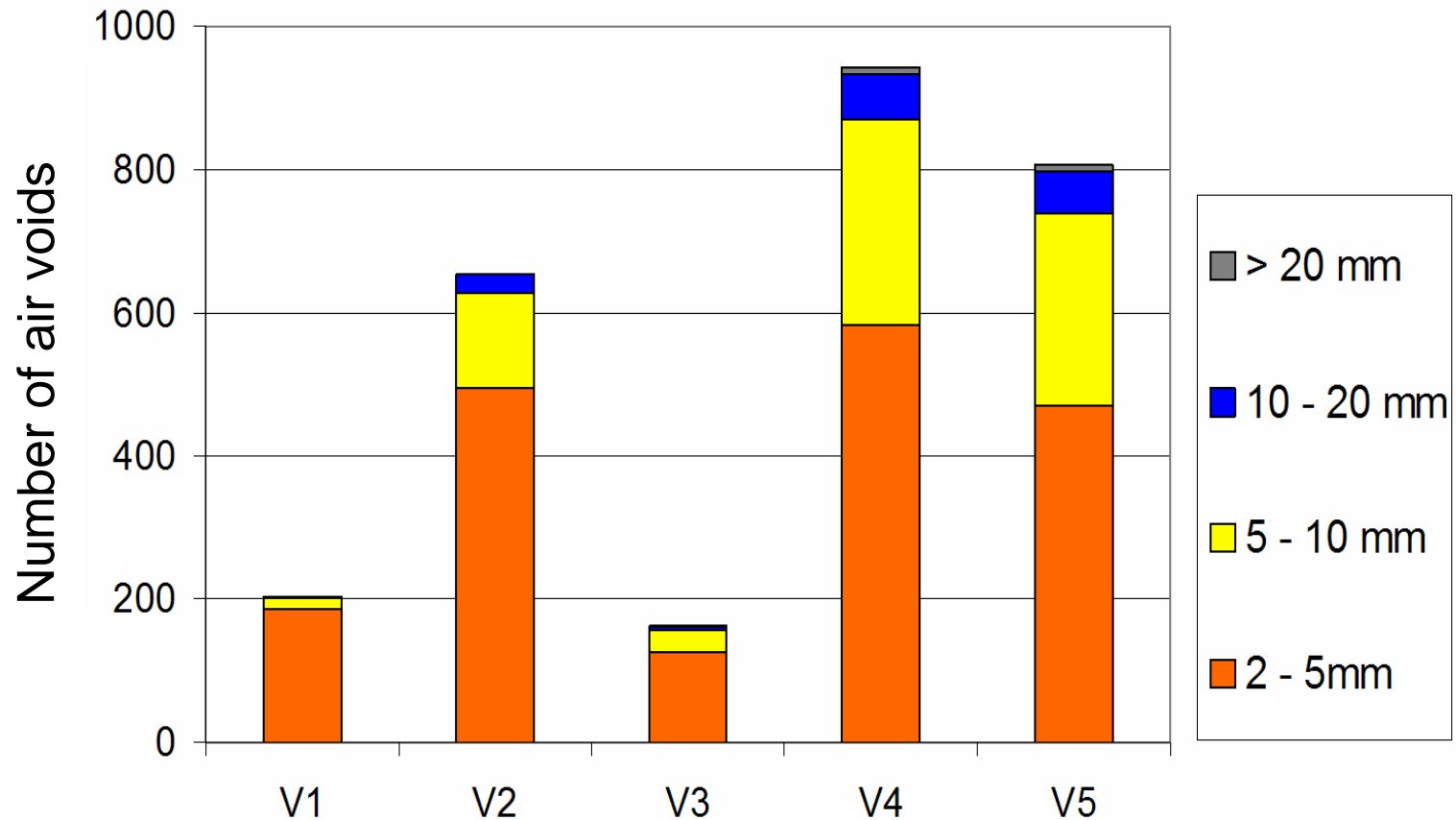
BPS-publication 24: *Typiske beskrivelsesafsnit – indvendige betonoverflader til malebehandling og tapetopsætning* (2. udgave, 1989).

For each wall four sections are chosen of 1x1 m². The sections represent

Results



Results



The surface finish is very dependent on the casting technique and the rheological properties.

Results

According to annex F in DS 2426 concrete in exposure class XF2, XF3 og XF4 (A, A and E in DS 481), which is exposed to a combination of salt and frost should obtain:

- Air void content in hardened concrete (DS/EN 480-11) $> 3,5\%$
- Spacing factor is < 0.20 .

It is observed that all the tested samples fulfil these requirements except for the three core samples in the bottom of V1 where the total air void content is 3.4%.

Results

According to annex F in DS 2426 concrete in exposure class XF2, XF3 and XF4 (A, A and E in DS 481), should obtain the result *good* in a frost/thaw test (SS 13 72 44).

The results show that a satisfactory frost resistance is obtained.