

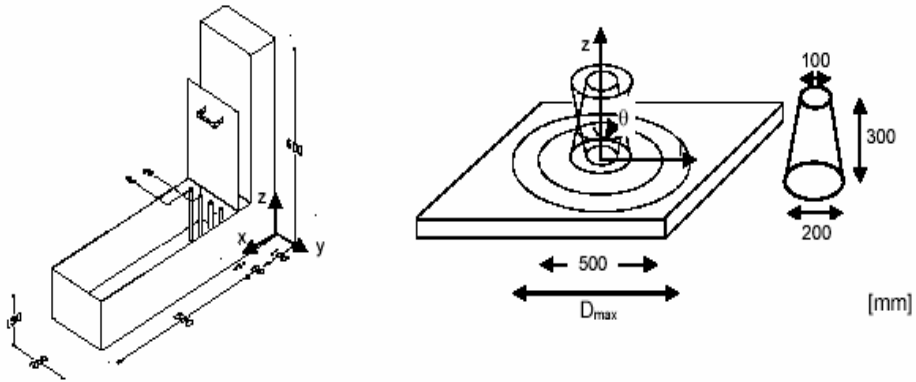
Simulation and Verification of Form Filling with Self-Compacting Concrete

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Objective

To verify a single fluid approach for simulation of SCC Form Filling

Approach - Part 1



Mass: $(\nabla \cdot \mathbf{v}) = 0$

Momentum: $\frac{\partial \rho \mathbf{v}}{\partial t} + \nabla \cdot (\rho \mathbf{v} \mathbf{v}) = -\nabla \cdot \boldsymbol{\sigma} + \rho \mathbf{g}$

$\boldsymbol{\sigma} = p\boldsymbol{\delta} + \boldsymbol{\tau}$ $\boldsymbol{\tau} = 2\eta\dot{\boldsymbol{\gamma}}$ $\eta = \eta_{pl} + \frac{\tau_0}{\dot{\boldsymbol{\gamma}}}$

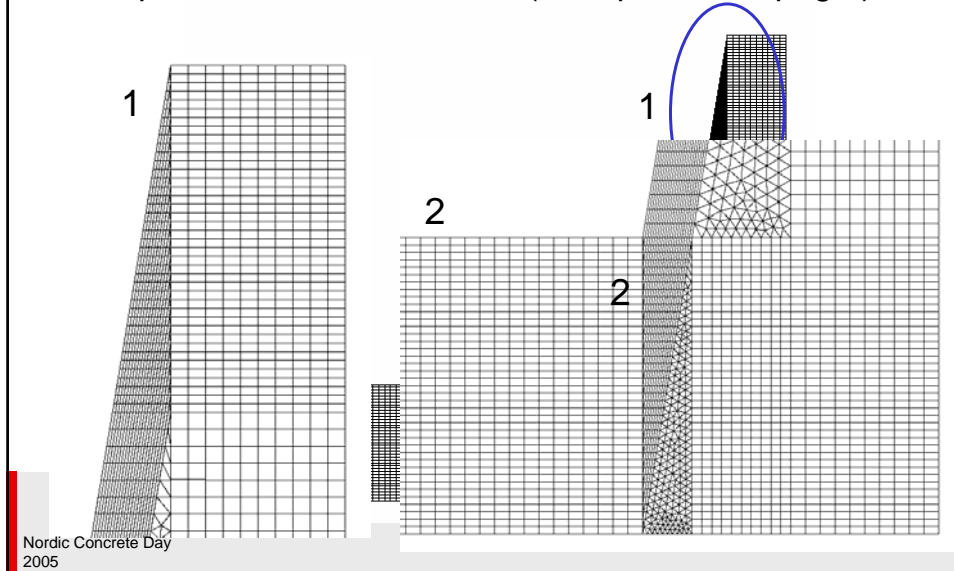
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Approach – Part 2: $l = 3 \text{ m}$, $w = 0.3 \text{ m}$, $h = 1 \text{ m}$

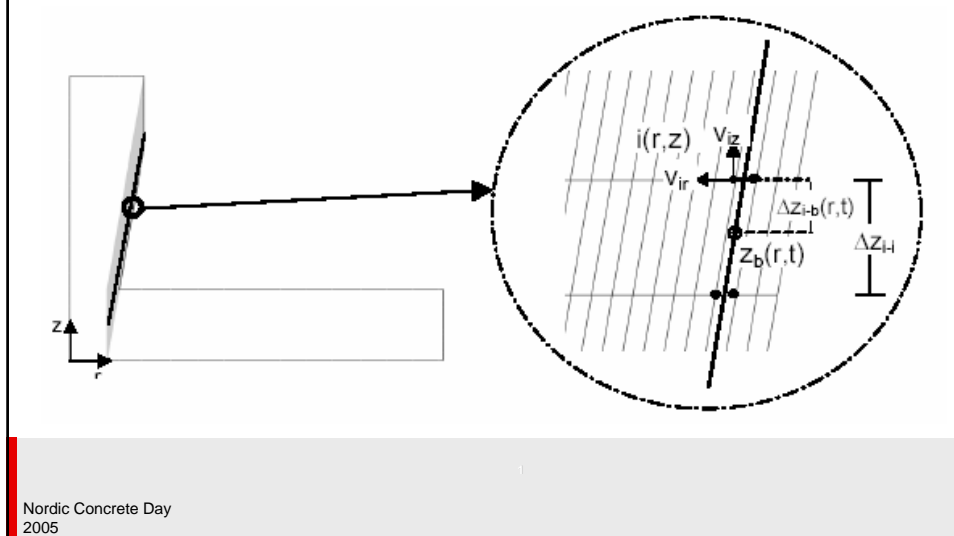


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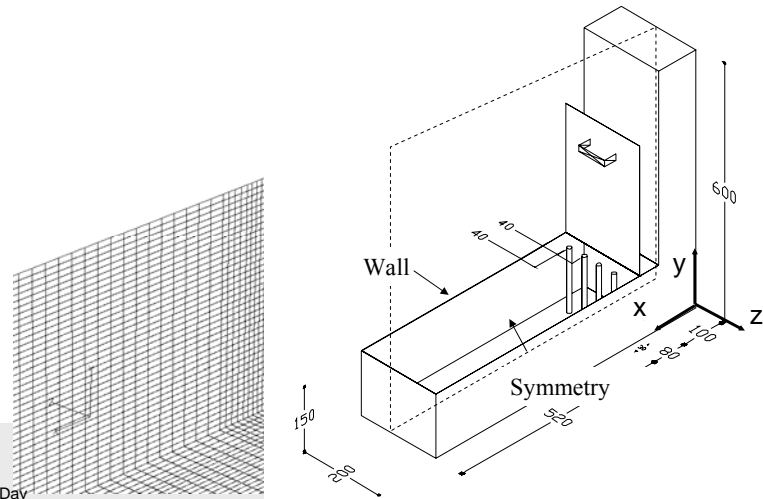
Computational Model - Part 1 (Slump Flow - Upright)



Computational Model - Part 1 (Slump Flow – Upside down)



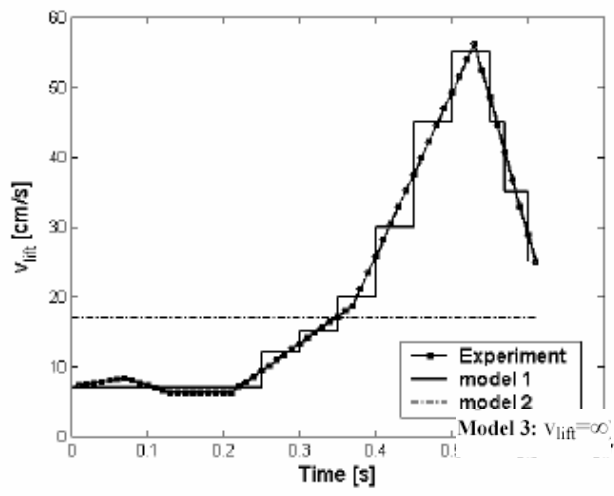
Computational Model – Part 1 (L-Box)



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Experimental – Part 1

- 1. A self-compacting
- BML Viscometer
- Slump Flow Test:
- L-Box



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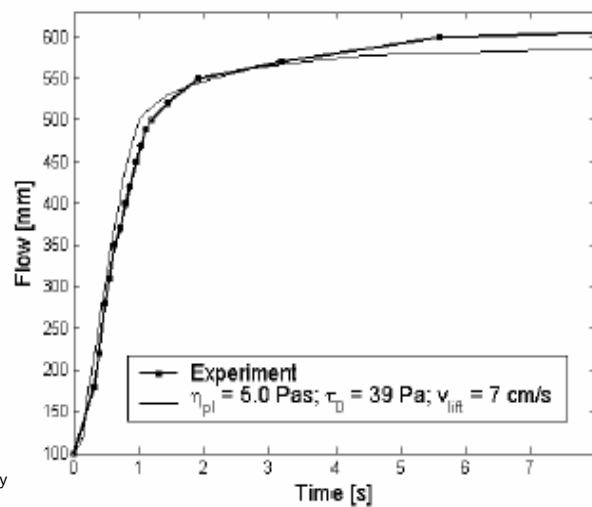
Experimental – Part 1

2. A self-compacting concrete

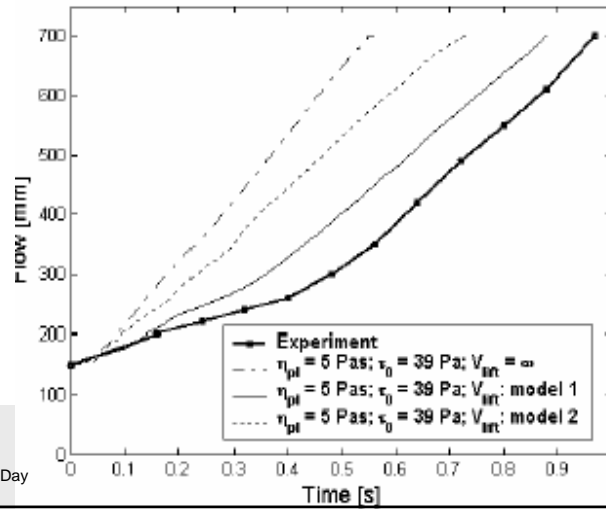
Slump Flow Test: $v_{\text{lift}} = 4 \text{ cm/s}$ – Upright

L-Box: $v_{\text{lift}} = 29 \text{ cm/s}$

Results – Part 1 (Slump Flow - Mortar)

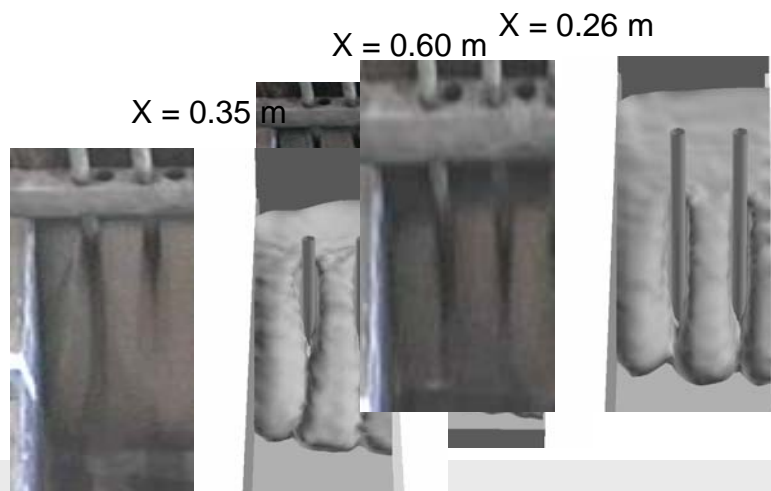


Results – Part 1 (L-Box - Mortar)



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Results – Part 1 (L-Box - Mortar)



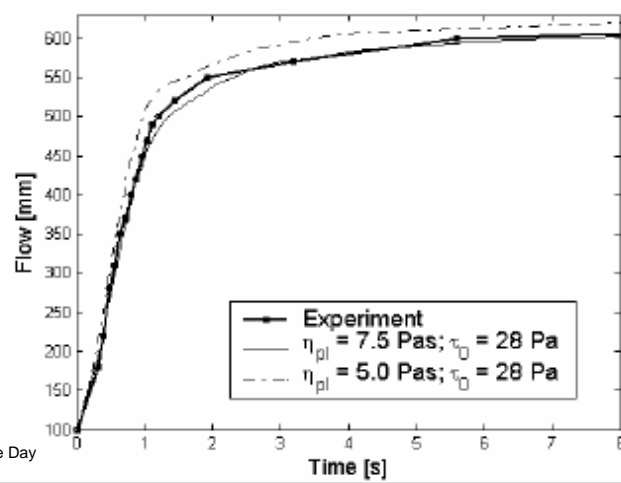
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Results – Part 1 (L- Box - Mortar)



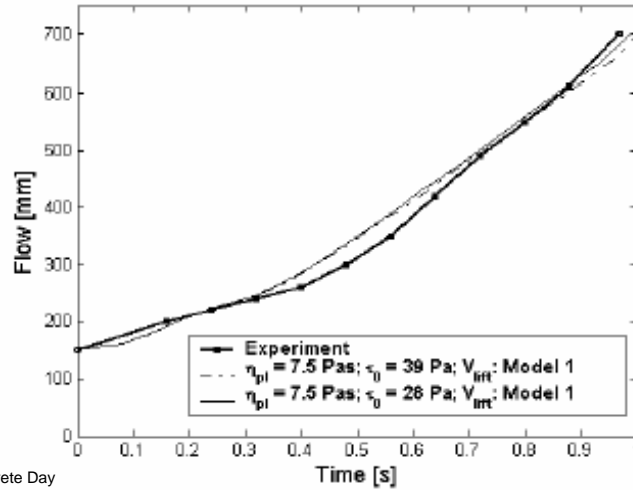
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Results – Part 1 (Slump Flow - Mortar)



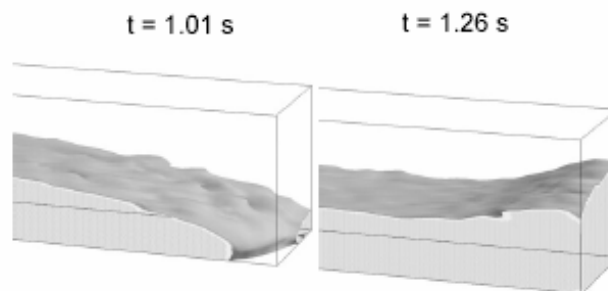
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Results – Part 1 (L-Box – Mortar)



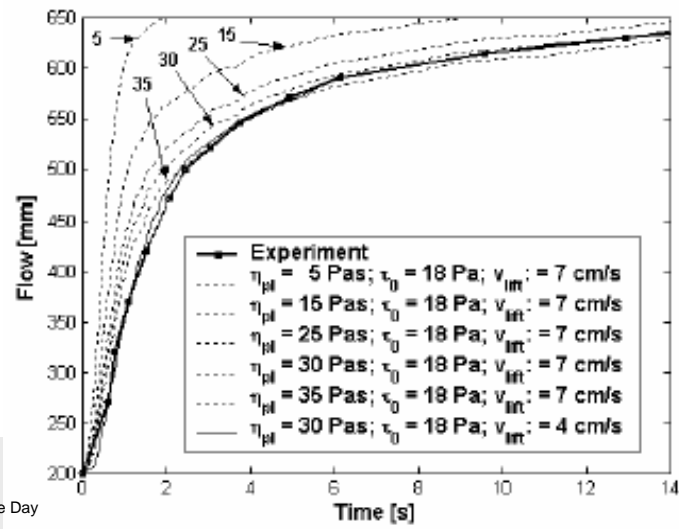
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Results – Part 1 (L-Box - Mortar)



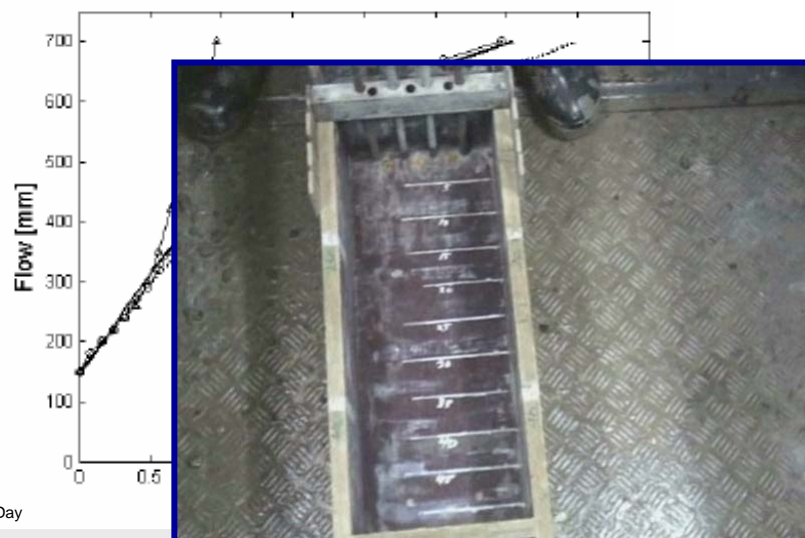
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Results – Part 1 (Slump Flow - Concrete)



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Results – Part 1 (L-Box – Concrete)



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Conclusion: Part 1

- Results show consistency between simulations and experiments for both the L-box and slump flow test for a given set of rheological properties when including moving boundaries and a reasonable agreement between rheological parameters determined in a viscometer and those applied to simulate flow is obtained.
- This indicate that the applied simulation approach could be valid for full-scale simulations.

Supplementary

- For assessment of rheological properties based on the test methods, complete control of the lifting velocity and a detailed and accurate monitoring of the transient flow behaviour are required.

4C Automatic Slump Flow



B/W Video camera

Lifting device – Ball screw ensures accurate lifting speed of 7 cm/s

Base plate in hardened sand blasted glass on adjustable rubber feet

Everything mounted on "rollers"

Monitor – one click and the analysis will proceed automatically

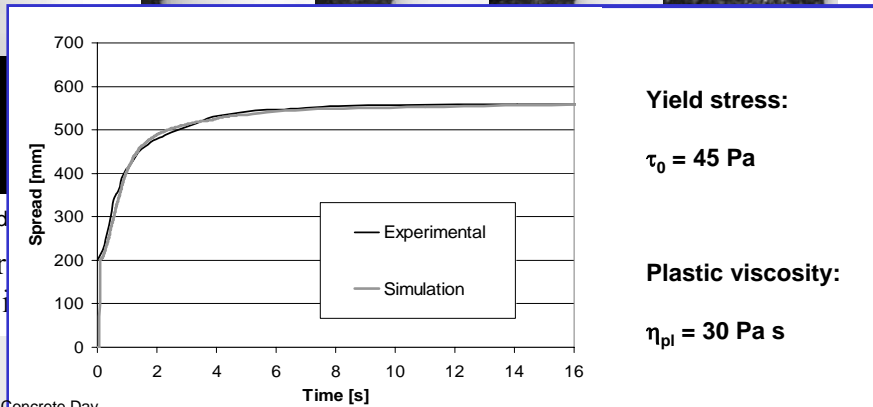
PC

Upright Abrams slump cone with weight ring

4C Automatic Slump Flow

Concept:

Raw image



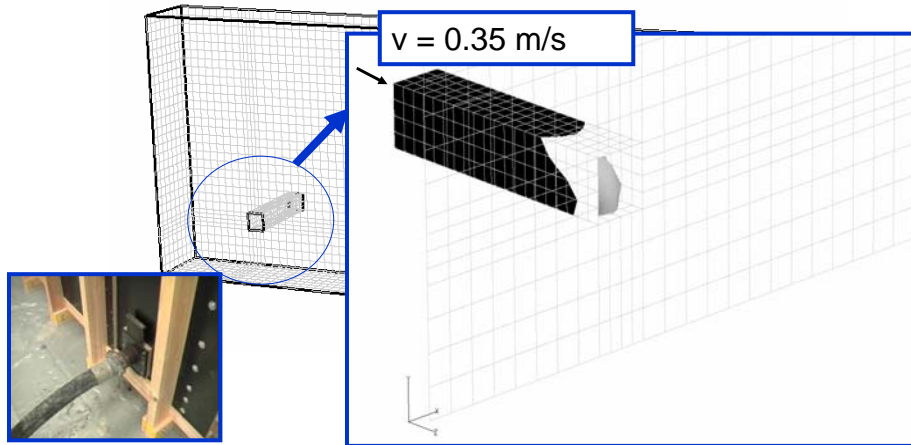
Yield stress:

$$\tau_0 = 45 \text{ Pa}$$

Plastic viscosity:

$$\eta_{pl} = 30 \text{ Pa s}$$

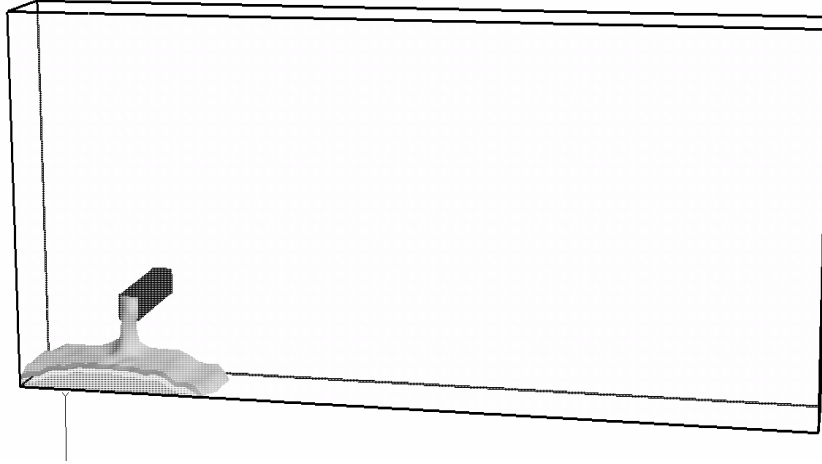
Computational Model – Part 2



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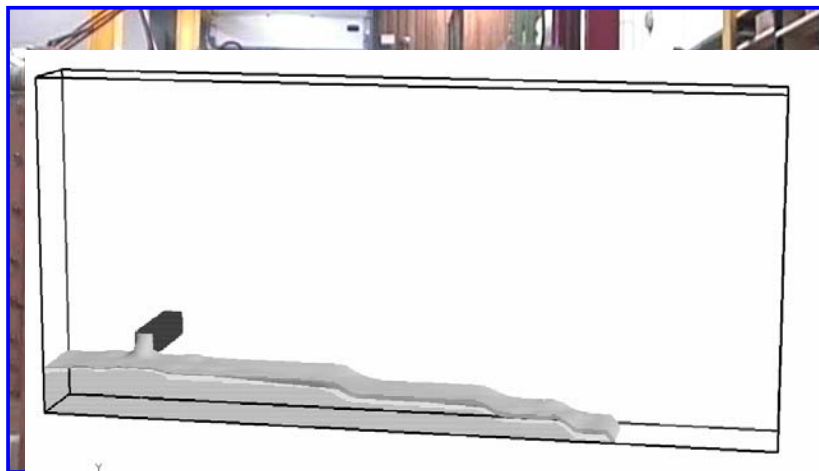


Results: Free Surface, Time = 6 s



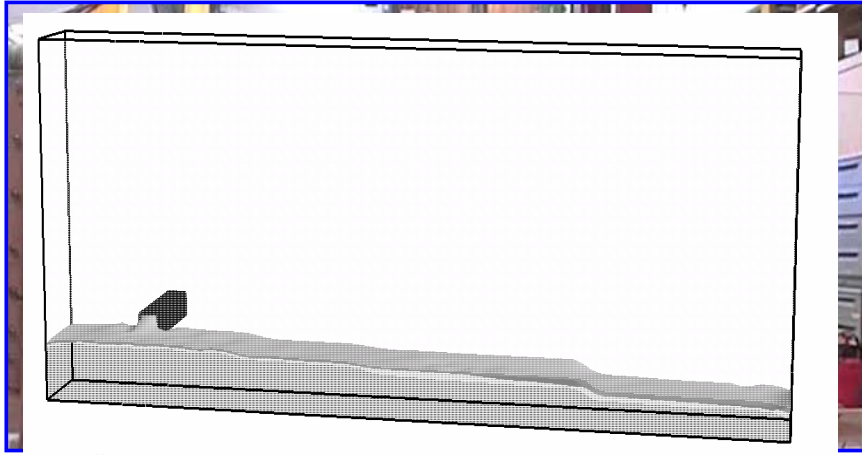
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Results: Free Surface, Time = 36 s



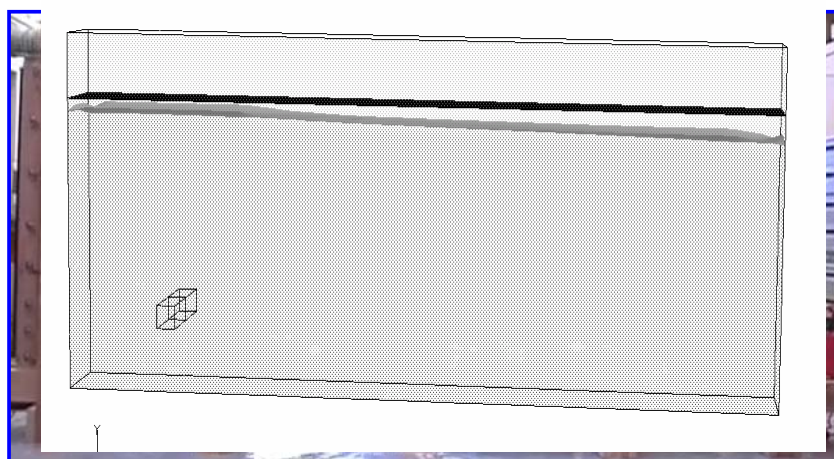
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Results: Free Surface, Time = 60 s



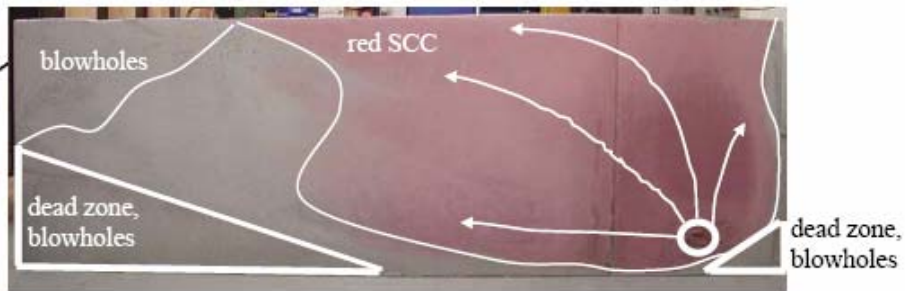
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Results: Free Surface, Time = 360 s



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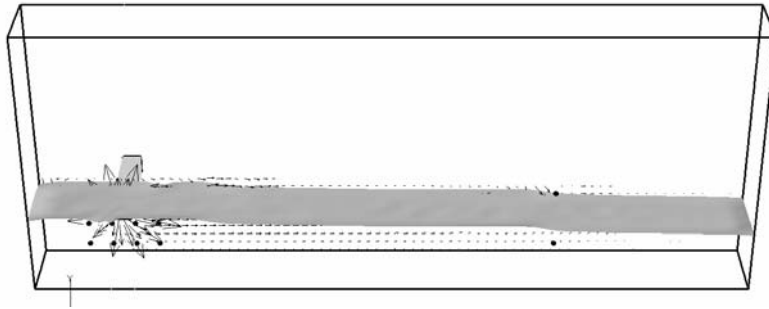
Results: Flow Patterns, Experimental, Side of inlet



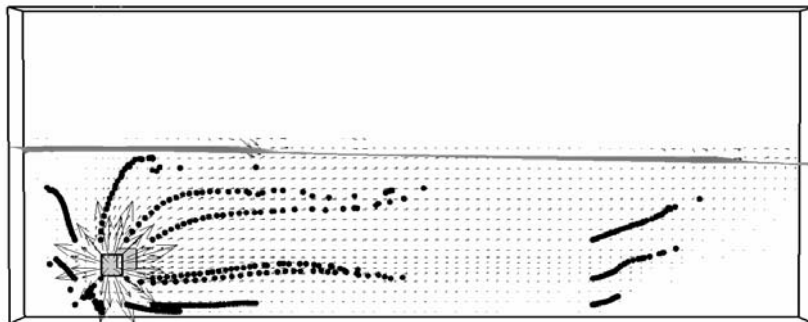
Results: Flow Patterns, Experimental, Side of inlet



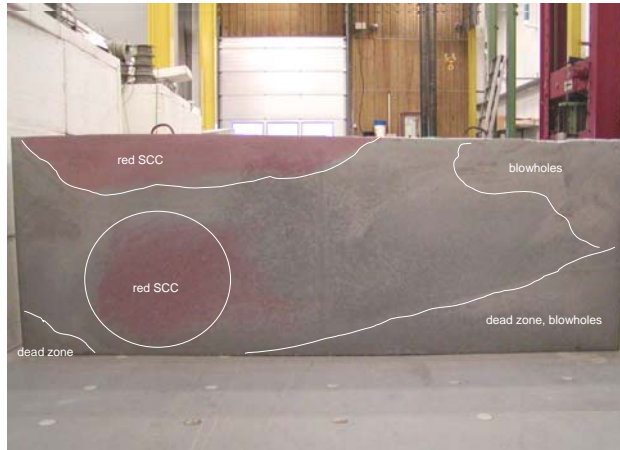
Results: Flow Patterns, Experimental, Side of inlet



Results: Flow Patterns, Experimental, Side of inlet

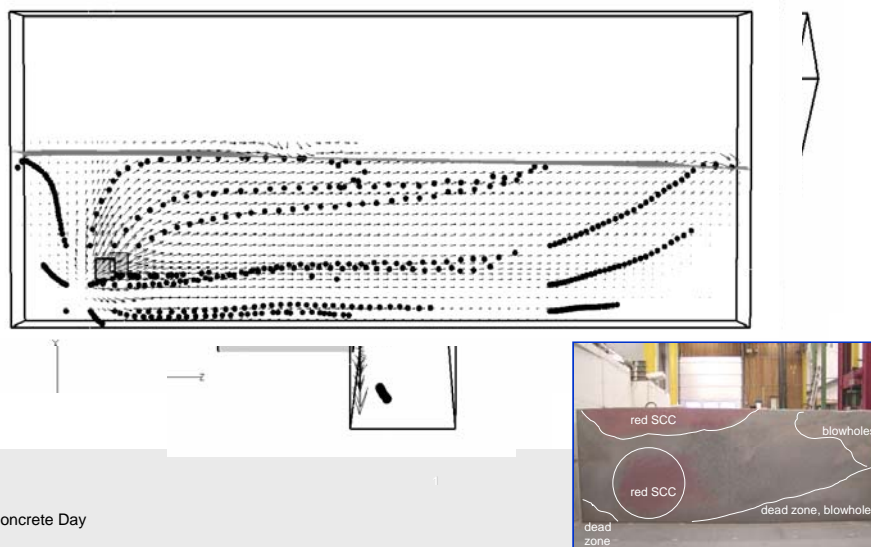


Results: Flow Patterns, Experimental, Transparent Side



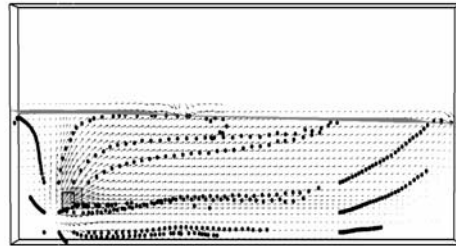
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RESULTS: Flow Patterns, Simulation, Transparent Side



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RESULTS: Flow Patterns



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Conclusions – Part 2

- Single fluid simulation of a Bingham fluid seem to capture the observations of the free surface and flow patterns observed in the form filling experiment.
- The flow patterns affect the dynamic segregation resistance
- The surface quality seems dependent on the shearing history at the formwork.

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